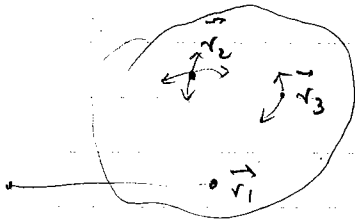


Rigid Bodies

? configuration
for a rigid body?

Coordinates for a rigid body



body within which
relative distances
do not change
approximation to real bodies
for weak forces
and coarse time-resolution
space

To position one chosen point, such as \vec{r}_1 ,
3 coordinates ^{are needed}. To position one more point
after that, e.g. \vec{r}_2 , 2 coordinates.

The second point can move on a
surface of a sphere of radius r_{21} .

After that, the points of the body
can still rotate on circles concentric
with the \vec{r}_{21} axis and we can restrain
that by specifying the position of
some point \vec{r}_3 with one coordinate.

After that, all points of the body
have fixed positions.

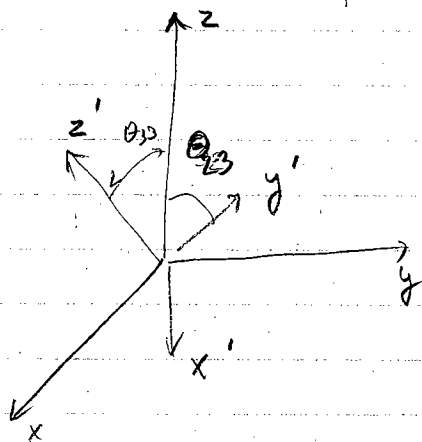
Altogether, we need 6 coordinates to
specify the configuration of a rigid body,
3 to specify the placement and 3
to specify orientation.

Constraints placed on a rigid body,
may reduce the number of needed
coordinates.

When describing ^{the} mass distribution within a rigid body, it is convenient to use cartesian coordinates in a system associated with the body. Within that system the distribution never changes.

However, the ^{body} coordinate axes will be generally oriented differently than ^{an} external system.

For the moment, we shall assume that the origins of the systems coincide.



' coordinate system associated with the body

unprimed external

unit vectors in the directions of the axes $\vec{i}, \vec{j}, \vec{k} \equiv \vec{u}_1, \vec{u}_2, \vec{u}_3$
 coordinates $x, y, z \equiv x_1, x_2, x_3$

$$\vec{r} = x\vec{i} + y\vec{j} + z\vec{k} \equiv \sum_e x_e \vec{u}_e \equiv x_e \vec{u}_e$$

Unless otherwise specified or an explicit summation sign is used, the repeated indices imply a summation over those indices

Simultaneously, we have

$$\vec{r} = x'_k \vec{u}'_k$$

Now

$$\vec{r} \cdot \vec{u}_k = x'_l \vec{u}'_l \cdot \vec{u}_k = x'_l \delta_{lk} = x'_k$$

$$\text{So } \vec{r} = (\vec{r} \cdot \vec{u}_l) \cdot \vec{u}_l$$

In particular

✓ angle between primed & unprimed axes

$$\vec{u}'_k = (\vec{u}'_k \cdot \vec{u}_l) \cdot \vec{u}_l = \cos \theta_{kl} \vec{u}_l$$

Now we have

$$\begin{aligned} \vec{u}'_k \cdot \vec{u}'_j &= \delta_{kj} = \cos \theta_{kl} \vec{u}_l \cdot \cos \theta_{jl} \vec{u}_i \\ &= \cos \theta_{kl} \cos \theta_{jl} \delta_{li} \\ &= \cos \theta_{kl} \cos \theta_{jl} \end{aligned}$$

$$k=j \Rightarrow 1 = \sum_l \cos^2 \theta_{kl} \quad 3 \text{ eqs}$$

$$k \neq j \Rightarrow 0 = \sum_l \cos \theta_{kl} \cos \theta_{jl} \quad \frac{2 \times 3}{2} = 3 \text{ eqs}$$

altogether $3 \times 3 = 9$ angles

Also

$$\vec{u}_k = (\vec{u}_k \cdot \vec{u}'_l) \vec{u}'_l = \cos \theta_{kl} \vec{u}'_l$$

$$\begin{aligned} \vec{u}_k \cdot \vec{u}_n &= \delta_{kn} = \cos \theta_{kl} \vec{u}'_l \cdot \cos \theta_{ln} \vec{u}'_m = \cos \theta_{kl} \cos \theta_{ln} \delta_{lm} \\ &= \sum_l \cos \theta_{kl} \cos \theta_{ln} \end{aligned}$$

Vector \vec{r}

$$x'_k = \vec{r} \cdot \vec{u}'_k = x_e \vec{u}_e \cdot \vec{u}'_k \\ = x_e \cos \theta_{ke}$$

Introducing a matrix \bar{A} with elements

$$A_{ke} = \cos \theta_{ke}$$

row
index

↑ ↑
column
index

$$\bar{A} = \begin{pmatrix} \cos \theta_{11} & \cos \theta_{12} & \cos \theta_{13} \\ \cos \theta_{21} & \cos \theta_{22} & \cos \theta_{23} \\ \cos \theta_{31} & \cos \theta_{32} & \cos \theta_{33} \end{pmatrix}$$

$$x'_k = A_{ke} x_e$$

$k=1,2,3$

this represents a linear transformation in 3 dim space
 \bar{A} is called a transformation mtr

We have

$$\sum_e A_{ke} A_{je} = \sum_e \cos \theta_{ke} \cos \theta_{je} = \delta_{jk}$$

$$\sum_e A_{ke} A_{je} = \delta_{jk}$$

A transformation with such a property is termed orthogonal

Also

$$\sum_k A_{ke} A_{kn} = \delta_{en}$$

Introducing a transposed matrix \bar{A}^T ,
such that

$$(\bar{A}^T)_{ij} = \bar{A}_{ji}$$

we can write the orthogonality condition
as

$$A_{ik} A_{ej}^T = \delta_{ij} \quad \text{or} \quad \bar{A} \bar{A}^T = \bar{I}$$

where \bar{I} is a unit matrix
also $\bar{A}^T \bar{A} = \bar{I}$

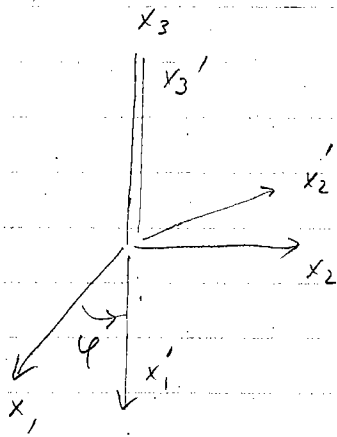
$$\bar{I} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

The orthogonality condition ensures
that the scalar products remain the
same no matter what the coordinate
system is used

$$\vec{x} = x_k u_k \quad \vec{y} = y_k u_k \quad \vec{x} \cdot \vec{y} = x_k y_k$$

$$\vec{x} \cdot \vec{y} = x'_k y'_k = A_{ke} x_e A_{kn} y_n = \delta_{en} x_e y_n = x_n y_n$$

Example: coordinate systems related by a rotation about the z -axis



$$x_1' = x_1 \cos \varphi + x_2 \sin \varphi$$

$$x_2' = -x_1 \sin \varphi + x_2 \cos \varphi$$

$$x_3' = x_3$$

$$A_{11} = \cos \varphi \quad A_{12} = \sin \varphi \quad A_{13} = 0$$

$$A_{21} = -\sin \varphi \quad A_{22} = \cos \varphi \quad A_{23} = 0$$

$$A_{31} = 0 \quad A_{32} = 0 \quad A_{33} = 1$$

$$\bar{A} = \begin{pmatrix} \cos \varphi & \sin \varphi & 0 \\ -\sin \varphi & \cos \varphi & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

Orthogonality $\sum_c A_{kc} A_{nc} = \delta_{kn}$?

$$k=n=1 \quad \cos^2 \varphi + \sin^2 \varphi + 0 = 1$$

$$k=n=2 \quad \sin^2 \varphi + \cos^2 \varphi + 0 = 1$$

$$k=n=3 \quad 0 + 0 + 1 = 1$$

$$k=1, n=2 \quad -\cos \varphi \sin \varphi + \sin \varphi \cos \varphi + 0 = 0$$

$$k=1, n=3 \quad 0 + 0 + 0 = 0$$

Transformation matrix as an operator

When the two coordinate systems coincide the coordinates for \vec{r} in the set \mathcal{O} and \mathcal{O}' are the same.

After the body rotation the coordinates in \mathcal{O}' stay the same while those in \mathcal{O} change. Thus we may view the relation

$$x'_k = A_{ke} x_e \quad \leftarrow \text{after rotation}$$

\uparrow before body rotation

as a rotation transformation

Using the orthogonality relation

$$A_{kh} x'_k = A_{kh} A_{ke} x_e = \delta_{he} x_e = x_h$$

$$A^T_{nk} x'_k = x_n$$

$$\vec{r} = \vec{A}^T (\vec{r}')'$$

$\underbrace{\hspace{2cm}}$ vector with coordinates such as in body frame

that vector gets rotated in the manner prescribed by \vec{A}^T to produce \vec{r}

Inverse Transformation

$$\theta \xrightarrow{A} \theta'$$

↙ A^{-1}

$$x'_i = A_{ik} x_k$$

$$x_k = A^{-1}_{kj} x'_j$$

$$x'_j = \delta_{jn}$$

$$x'_i = A_{ik} A^{-1}_{kj} x'_j$$

$$\Rightarrow A_{ik} A^{-1}_{kj} = \delta_{ij}$$

$$\bar{A} \bar{A}^{-1} = \bar{I}$$

$$x_k = A^{-1}_{kj} A_{ji} x_i$$

$$\Rightarrow A^{-1}_{kj} A_{ji} = \delta_{ki}$$

$$\bar{A}^{-1} \bar{A} = \bar{I}$$

We have

$$\bar{A}^{-1} \bar{A} = \bar{A}^T \bar{A}$$

$$A_{jk} A_{ik} = \delta_{ji}$$

$$A_{jk} A^T_{ki} = \delta_{ji}$$

$$\bar{A}^T = \bar{A}^{-1}$$

Inverse of an orthogonal matrix is equal to the transpose of the matrix.

equivalent def.

Other special matrices

$$\bar{A}^T = \bar{A}$$

$$\Leftrightarrow A_{ij} = A_{ji}$$

symmetric

$$\bar{A}^T = -\bar{A}$$

$$\Leftrightarrow A_{ij} = -A_{ji}$$

antisymmetric

note: diagonal elements of antisymmetric mtr $A_{ii} = 0 \quad i = 1, 2, 3$

Superposition of transformations

$$\Theta \rightarrow \Theta' \rightarrow \Theta''$$

$$x'_k = B_{kj} x_j$$

$$x''_i = A_{ik} x'_k = A_{ik} B_{kj} x_j$$

$$x''_i = C_{ij} x_j$$

$$C_{ij} = A_{ik} B_{kj}$$

The transformation matrix

$$\bar{C} = \bar{A} \cdot \bar{B}$$

The multiplication is not commutative,
i.e. generally $\bar{B} \cdot \bar{A} \neq \bar{A} \bar{B}$.

However, the multiplication is associative

$$\Theta \xrightarrow{C} \Theta' \xrightarrow{B} \Theta'' \xrightarrow{A} \Theta'''$$

$$\bar{D} = \bar{A} \cdot \bar{B} \cdot \bar{C} = \bar{A} (\bar{B} \cdot \bar{C}) = (\bar{A} \cdot \bar{B}) \cdot \bar{C}$$

$$D_{ij} = (A_{ik} B_{ke}) C_{ej}$$

demonstrate noncomm

Transformation of linear operators

Let us consider a linear operator within one coordinate system, \mathcal{O} ,

Examples: multiplication by a constant, rotation, projection on an axis, etc.

$$y_i = F_{ik} x_k \quad \mathcal{O}$$

How does the operator transform under the change of the coordinate system?

$$y'_j = F'_{je} x'_e \quad \mathcal{O}'$$

Relation between F' and F ?

$$A_{jn} y_n = F'_{je} A_{em} x_m$$

$$A_{jn} F_{nk} x_k = F'_{je} A_{em} x_m \quad x_k = \delta_{ks}$$

$$A_{jn} F_{ns} = F'_{je} A_{es} \quad \times A_{su}^{-1}$$

$$A_{jn} F_{ns} A_{su}^{-1} = F'_{ju} \quad \Rightarrow \quad \bar{F}' = \bar{A} \bar{F} \bar{A}^{-1}$$

$$\bar{I}' = \bar{A} \bar{I} \bar{A}^{-1} = \bar{I}$$

Determinants

$$|\bar{A}|$$

$$|\bar{A} \cdot \bar{B}| = |\bar{A}| \cdot |\bar{B}|$$

$$|\bar{I}| = 1 \quad |\bar{A}^T| = |\bar{A}|$$

$$1 = |\bar{I}| = |\bar{A} \bar{A}^{-1}| = |\bar{A}| |\bar{A}^{-1}|$$

$$|\bar{A}| = |\bar{A}^T| = |\bar{A}^{-1}| = |\bar{A}|^{-1}$$

↑

for an orthogonal matrix $1 = |\bar{A}|^2 \Rightarrow |\bar{A}| = \pm 1$

Only transformations with $|\bar{A}| = +1$ can represent rotations

✓ A rotation may be represented as a superposition of tiny rotations

$$\bar{A} = A_1 \cdots A_n$$

↑ ↑
tiny rotations, nearly \bar{I}
must have $|\bar{A}_i| = 1$

$$\Rightarrow |\bar{A}| = 1$$

Transformations with $|\bar{A}| = -1 \Rightarrow$ rotations followed

by a reflection. Eg

↓ change handedness of a coordinate system

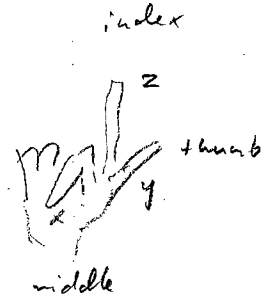
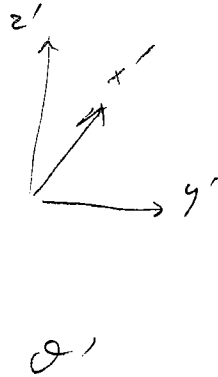
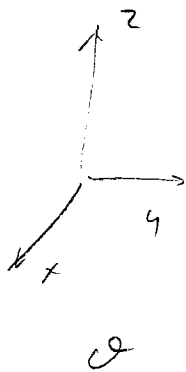
$$\begin{pmatrix} -1 & 0 \\ 0 & 1 \end{pmatrix}$$

$$x' = -x$$

$$y' = y$$

$$z' = z$$

~~cannot be accomplished~~

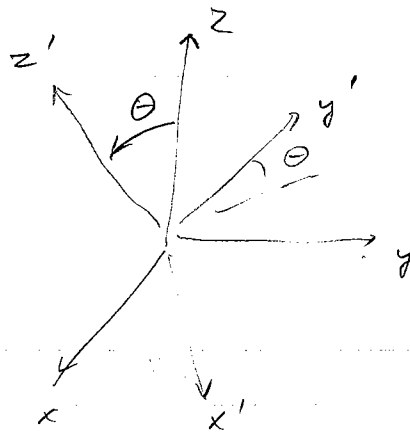
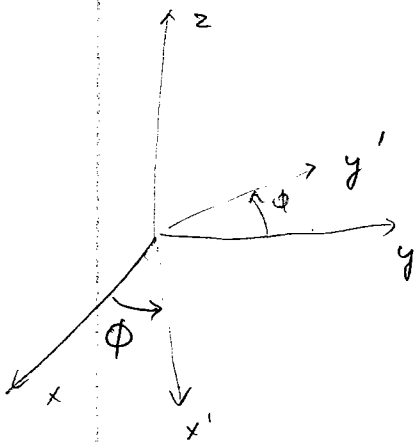


Right-handed system turned into left-handed

Euler Angles

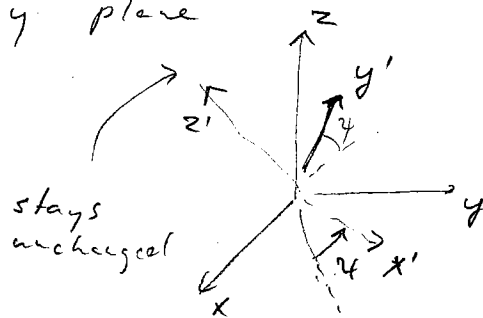
3 parameters sufficient to specify a general rotation transformation from Q to Q'

One choice: Euler angles



z stays unchanged

But still x' stays with xy plane
 Can't be most general
 Final rotation by ψ around z'



Full transformation matrix

$$\vec{A} = \vec{B} \vec{C} \vec{D}$$

↑ ↑ ↑
3 rotations

$$\vec{D} = \begin{pmatrix} \cos \phi & \sin \phi & 0 \\ -\sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$\vec{C} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & \sin \theta \\ 0 & -\sin \theta & \cos \theta \end{pmatrix}$$

$$\vec{B} = \begin{pmatrix} \cos \psi & \sin \psi & 0 \\ -\sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

Inverse transformation matrix

$$\bar{A}^{-1} = \bar{D}^{-1} \bar{C}^{-1} \bar{B}^{-1} = \bar{D}^T \bar{C}^T \bar{B}^T$$

Euler's theorem: The general displacement of a rigid body with one point fixed is a rotation about some axis.

\mathcal{O} external
 \mathcal{O}' body-fixed

fixed point - With regard to coordinate systems \mathcal{O} & \mathcal{O}' centered at the fixed point - any transf. from \mathcal{O} to \mathcal{O}' just a single rotation

change from one coordinate set to another with the same origin can be represented as a rotation about an axis \rightarrow any vector along that axis would have the same components in the two systems

e.g. z axis
y axis
x axis
or any other
- axis
- angle of rotation

With $\vec{r} = (x_1, x_2, x_3)$

and $\vec{r}' = (x'_1, x'_2, x'_3)$

For any \bar{A} a vector \vec{r} must exist such that

$$\vec{r}' = \bar{A} \vec{r} = \vec{r}$$

I.e. any transformation matrix must have an eigenvector with

$$\bar{A} \vec{r} = \lambda \vec{r}$$

with an eigenvalue 1, $\lambda = 1$.

I.e.

$$(\bar{A} - \lambda \bar{I}) \vec{r} = 0 \Leftrightarrow |\bar{A} - \lambda \bar{I}| = 0$$

$$\begin{vmatrix} a_{11} - \lambda & a_{12} & a_{13} \\ a_{21} & a_{22} - \lambda & a_{23} \\ a_{31} & a_{32} & a_{33} - \lambda \end{vmatrix} = 0$$

A 3-order polynomial has 3 solutions $\lambda_1, \lambda_2, \lambda_3$, corresponding to three eigenvectors $\vec{u}_1, \vec{u}_2, \vec{u}_3$ orthogonal

$$\vec{A} \vec{u}_k = \lambda_k \vec{u}_k \quad \text{with component of the } k^{\text{th}} \text{ vector}$$

$$A_{in} u_{nk} = \lambda_k u_{ik} \quad \leftarrow \text{no summation over } k$$

\uparrow k^{th} vector

Constructing a matrix \vec{V}

$$V_{nk} = u_{nk}$$

we can represent the eigenvalue eqs as

$$A_{in} V_{nk} = V_{ij} \delta_{jk} \lambda_k$$

and on applying \vec{V}^{-1} we can accomplish a diagonalization of \vec{A}

$$V_{mi}^{-1} A_{in} V_{nk} = V_{mi}^{-1} V_{ij} \delta_{jk} \lambda_k = \delta_{mk} \lambda_k$$

$$\vec{V}^{-1} \vec{A} \vec{V} = \begin{pmatrix} \lambda_1 & 0 & 0 \\ 0 & \lambda_2 & 0 \\ 0 & 0 & \lambda_3 \end{pmatrix}$$

$$\lambda_1 \lambda_2 \lambda_3 = |\vec{V}^{-1}|^{-1} |\vec{A}| |\vec{V}| = |\vec{A}| = 1$$

3 eigenvectors, As the transformation preserves distances, then a unit vector should remain a unit vector after the transformation, so $\lambda_k = 1$??
 But then $\vec{A} \equiv \vec{I}$. Any t. matrix should be identical to \vec{I}
 Where's the mistake in reasoning?? λ 's & u 's

might be complex! So we might have

$$\lambda_1 \lambda_2 \lambda_3 = 1 \quad \text{out of 3 complex eigenvalues}$$

corresponding to 3 complex vectors a move in real space

only rotations by 90° can be represented with such reflections

cases
 $\lambda = 1$
 $\lambda = -1 \times 2$
 or every 90°
 reflections

This is the situation in 2D,

??

$$(\bar{A} - \bar{I}) \bar{A}^T = \bar{I} - \bar{A}^T$$

$$|\bar{A} - \bar{I}| |\bar{A}^T| = |\bar{I} - \bar{A}^T|$$

$$|\bar{A} - \bar{I}| = |\bar{I} - \bar{A}|$$

Generally: $|\bar{B}| = (-1)^n |\bar{B}|$ where n is the dimension of the space

In 3D $|\bar{I} - \bar{A}| = (-1)^3 |\bar{A} - \bar{I}|$

With $|\bar{A} - \bar{I}| = -|\bar{I} - \bar{A}| \Rightarrow |\bar{A} - \bar{I}| = 0$

$$0 = |1 - (\lambda_1 - 1)(\lambda_2 - 1)(\lambda_3 - 1)|$$

Thus, there must be a unit eigenvalue & the Euler theorem is proven.

If we take $\lambda_3 = 1$ what about λ_1 & λ_2 ?

For \bar{A} real, if λ is a solution of $|\bar{A} - \lambda \bar{I}| = 0$, then also λ^* is, so $\lambda_2 = \lambda_1^*$

We also have $\lambda_1 \lambda_2 = 1 \Rightarrow \lambda_1 \lambda_1^* = 1$

$$\Rightarrow |\lambda_1|^2 = 1 \Rightarrow \lambda_1 = e^{i\Phi}, \lambda_2 = e^{-i\Phi}$$

$$\text{Tr } \bar{A} = \lambda_1 + \lambda_2 + \lambda_3 = 2 \cos \Phi + 1$$

What is Φ ?

In the vector basis, where the 3rd points along the invariant axis, the mtrx

$$\vec{A}' = \begin{pmatrix} \cos\Phi & \sin\Phi & 0 \\ -\sin\Phi & \cos\Phi & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

2 angles used
to orient \vec{n}
+ angle of
rotation
around

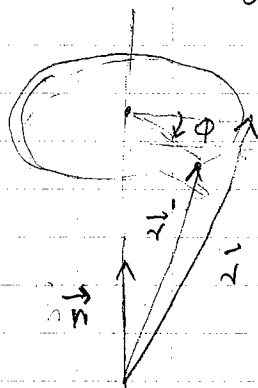
$$\text{Tr } \vec{A}' = 2\cos\Phi + 1$$

← now

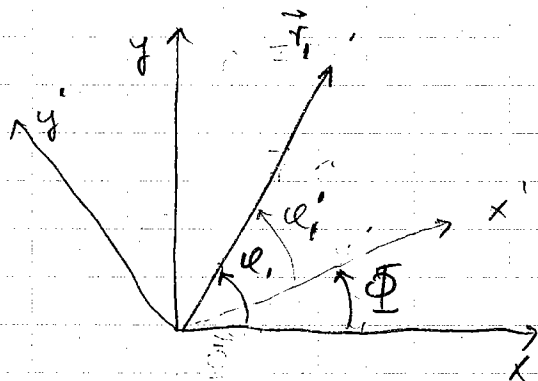
⇒ Φ is angle of rotation about the axis

↳ the angle, up to the sign, can
be obtained from the trace ...

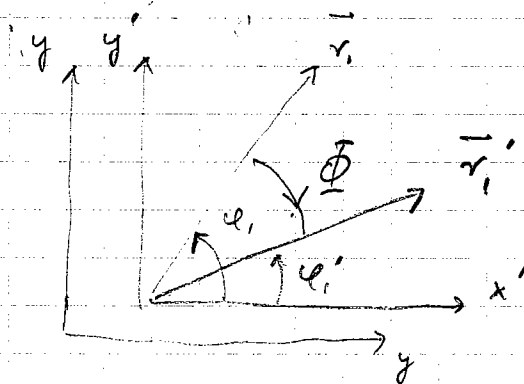
coordinate transform in terms of \vec{n} and Φ



When a coordinate system
is rotated one way,
then the vector, relative to
coordinates is rotated
the other way.



In the
frame
of the
axes
the coordinate
vectors



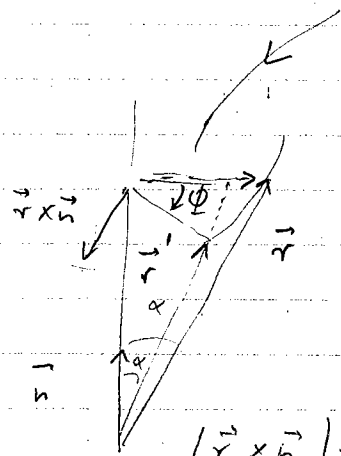
Coordinate transformation in terms of the axis and angle

$$\vec{r}' = (x_1', x_2', x_3')$$

$$\vec{r} = (x_1, x_2, x_3)$$

Three orthogonal axes in terms of \vec{n} & \vec{r}

$$\vec{e}_1, \quad \vec{r} - (\vec{n} \cdot \vec{r})\vec{n}, \quad \vec{r} \times \vec{n}$$



$$\vec{r}' = \vec{n}(\vec{n} \cdot \vec{r}) + (\vec{r} - (\vec{n} \cdot \vec{r})\vec{n}) \cos \Phi + (\vec{r} \times \vec{n}) \sin \Phi$$

$$|\vec{r} \times \vec{n}| = r \sin \alpha$$

$$|\vec{r} - (\vec{n} \cdot \vec{r})\vec{n}| = r \sin \alpha$$

$$\vec{r}' = \vec{r} \cos \Phi + \vec{n}(\vec{n} \cdot \vec{r})(1 - \cos \Phi) + (\vec{r} \times \vec{n}) \sin \Phi$$

Rotation formula

? Rotation angle in terms of Euler formulas

Trace of a matrix does not depend on the basis for a matrix

$$\text{Tr } \vec{A}' = \text{Tr } \vec{A} = \text{Tr}(\vec{B} \vec{C} \vec{D})$$

||

↑ ↑
in terms of Euler angles

$$\rightarrow \cos \frac{\Phi}{2} = \cos \frac{\Phi + \Psi}{2} \cos \frac{\Theta}{2}$$

Rotations from Superpositions of Infinitesimal Transformations

depends on the axis of rotation

$$x'_k \approx x_k + \underbrace{\epsilon_{ki} x_i}_{\text{small addition}} = (\delta_{ki} + \epsilon_{ki}) x_i$$

In vector form

$$\vec{x}' = (\bar{1} + \bar{\epsilon}) \vec{x}$$

Two infinitesimal rotations: $\bar{1} + \bar{\epsilon}_1$ & $\bar{1} + \bar{\epsilon}_2$

$$(\bar{1} + \bar{\epsilon}_1)(\bar{1} + \bar{\epsilon}_2) = \bar{1}^2 + \bar{1}\bar{\epsilon}_2 + \bar{1}\bar{\epsilon}_1 + \bar{\epsilon}_1\bar{\epsilon}_2$$

$$= \bar{1} + \bar{\epsilon}_1 + \bar{\epsilon}_2 = (\bar{1} + \bar{\epsilon}_2)(\bar{1} + \bar{\epsilon}_1)$$

↑ to the lowest order

Infinitesimal rotations commute, in contrast to those for finite angle

In general $\bar{B}\bar{C} \neq \bar{C}\bar{B}$

For a rotation over 3 infinitesimal Euler angles

$$\bar{A} = \begin{pmatrix} 1 & d\varphi & 0 \\ -d\varphi & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & d\theta \\ 0 & -d\theta & 1 \end{pmatrix} \begin{pmatrix} 1 & d\psi & 0 \\ -d\psi & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$= \begin{pmatrix} 1 & d\psi + d\varphi & 0 \\ -d\psi - d\varphi & 1 & d\theta \\ 0 & -d\theta & 1 \end{pmatrix} \Rightarrow \bar{\epsilon} = \begin{pmatrix} 0 & d\psi + d\varphi & 0 \\ -d\psi - d\varphi & 0 & d\theta \\ 0 & -d\theta & 0 \end{pmatrix}$$

If $\bar{A} = \bar{I} + \bar{E}$, then $\bar{A}^{-1} = \bar{I} - \bar{E}$, because

$$\bar{A} \bar{A}^{-1} = (\bar{I} + \bar{E})(\bar{I} - \bar{E}) = \bar{I} - \cancel{\bar{E}} + \cancel{\bar{E}} - \bar{E}^2 = \bar{I}$$

Since

$$\bar{A}^{-1} = \bar{A}^T \Leftrightarrow \bar{I} - \bar{E} = \bar{I} + \bar{E}^T$$

we must have

$$\bar{E}^T = -\bar{E},$$

i.e. the matrix \bar{E} is antisymmetric.
Without the loss of generality, we may represent it as

$$\bar{E} = \begin{pmatrix} 0 & d\Omega_3 & -d\Omega_2 \\ -d\Omega_3 & 0 & d\Omega_1 \\ d\Omega_2 & -d\Omega_1 & 0 \end{pmatrix}$$

$$\vec{r}' - \vec{r} = d\vec{r} = \bar{E} \vec{r}$$

$$dx_1 = x_2 d\Omega_3 - x_3 d\Omega_2$$

$$dx_2 = x_3 d\Omega_1 - x_1 d\Omega_3$$

$$dx_3 = x_1 d\Omega_2 - x_2 d\Omega_1$$

$$d\vec{r} = \vec{r} \times d\vec{\Omega}$$

What is $d\vec{\Omega}$?

Rotation formulae for small $d\phi$

$$\cos d\phi \approx 1, \quad \sin d\phi \approx d\phi$$

$$\vec{r}' = \vec{r} + (\vec{r} \times \vec{n}) d\phi$$

$$d\vec{r} = \vec{n} \times \vec{r} d\phi$$

$$d\vec{r} = \vec{r} \times d\vec{r} = -d\vec{r} \times \vec{r}$$

$$\vec{E} = d\Omega_k \vec{M}_k = d\phi \cdot n_k \vec{M}_k$$

$$\vec{M}_1 = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 1 & 0 \end{pmatrix} \quad \vec{M}_2 = \begin{pmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ -1 & 0 & 0 \end{pmatrix}$$

$$\vec{M}_3 = \begin{pmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

Infinitesimal rotation generators

$$d\Omega_k M_{ijk} r_j$$

If we write

$$(d\vec{r} \times \vec{r})_i = \epsilon_{ijk} d\Omega_k r_j = -d\Omega_k \epsilon_{ijk} r_j$$

where ϵ_{ijk} is the permutation symbol, equal to 0 when any 2 indices are equal and otherwise either +1 or -1, if ijk is an even or odd permutation of 1, 2, 3, then

$$M_{ijk} = -\epsilon_{ijk}$$

↑
kth mth nth

3 2 1 or

$$\vec{E} = -d\phi \vec{n} \cdot \vec{M}$$

3rd rank tensor

Changes in the vector during rotation

$$\epsilon_{ij} = +d\phi n_k \epsilon_{ijk}$$

$$dr_i = \epsilon_{ij} r_j = d\phi n_k \epsilon_{ijk} r_j$$

$$\frac{dr_i}{d\phi} = (\epsilon_{ijk} n_k) r_j = N_{ij} r_j$$

try to jump this

$$\frac{d\vec{r}}{d\phi} = \vec{N} \vec{r}$$

$$\vec{N} = -n_k \vec{M}_k = -\vec{n} \vec{M}$$

\hat{z} axis can change during rotation

Note:

- #1 Above transformations refer to a case when the coordinate system is rotated by an angle $d\phi$. The vector, as perceived in the coordinate system, rotates by $-d\phi$. If an active rotation of the vector is done then the above results hold with $d\phi \rightarrow -d\phi$.

In particular

$$d\vec{r} = d\vec{\Omega} \times \vec{r}$$

- #2 If improper transformations, $|\vec{A}| = -1$, are allowed then $d\vec{\Omega}$ transforms differently than vectors. Thus under an inversion

$$\vec{S} = -\vec{I} = \begin{pmatrix} -1 & & 0 \\ & -1 & \\ 0 & & -1 \end{pmatrix}$$

$$r'_k = A_{ki} r_i$$

$$d\Omega'_k = |\vec{A}| A_{ki} d\Omega_i$$

pseudovector

$$r'_k = S_{ki} r_i = -r_k$$

$$dr'_k = S_{ki} dr_i = -dr_k$$

$$\Rightarrow d\Omega'_i = d\Omega_i \quad dr_k = \epsilon_{klj} d\Omega_j r_e$$

$$-dr_k = \epsilon_{klj} d\Omega'_j (-r_e)$$

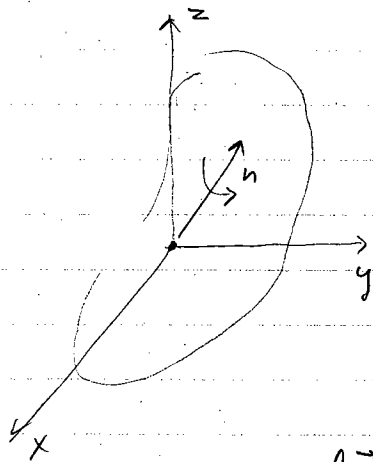
#3 The infinitesimal rotation operators satisfy commutation rules

$$\bar{M}_i \bar{M}_j - \bar{M}_j \bar{M}_i \equiv [\bar{M}_i, \bar{M}_j] = \epsilon_{ijk} \bar{M}_k$$

$[,]$ - commutator

$$[\bar{A}, \bar{B}] = \bar{A}\bar{B} - \bar{B}\bar{A}$$

Rate of change as a body rotates



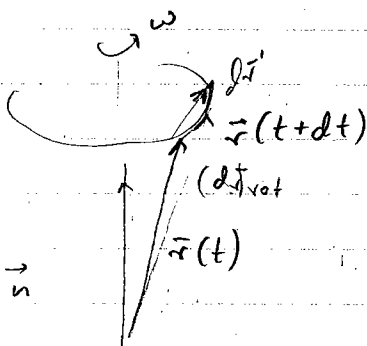
$\vec{r}' = (x_1', x_2', x_3')$ body fixed frame

$\vec{r} = (x_1, x_2, x_3)$ external frame

body rotates about a common center for the coordinates

$$d\vec{r} = d\vec{r}' + (d\vec{r})_{\text{rot}}$$

↑ true even when $d\vec{r}' = 0$



$$(d\vec{r})_{\text{rot}} = d\vec{\Omega} \times \vec{r}$$

$$d\vec{r} = d\vec{r}' + d\vec{\Omega} \times \vec{r}$$

$$\left. \frac{d\vec{r}}{dt} \right|_{\mathcal{O}} = \left. \frac{d\vec{r}'}{dt} \right|_{\mathcal{O}'} + \frac{d\vec{\Omega}}{dt} \times \vec{r}$$

$$\vec{v} = \vec{v}' + \vec{\omega} \times \vec{r}$$

This will be valid for any vector compared in the 2 frames, not just position

$$(d\vec{G})_{\mathcal{O}} = (d\vec{G})_{\mathcal{O}'} + (d\vec{G})_{\text{rot}} = (d\vec{G})_{\mathcal{O}'} + d\vec{\Omega} \times \vec{G}$$

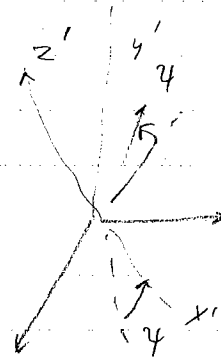
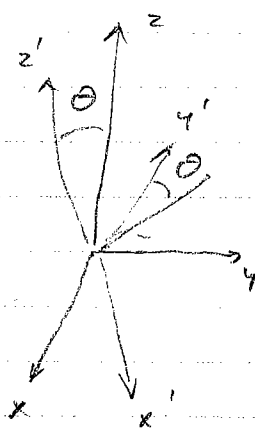
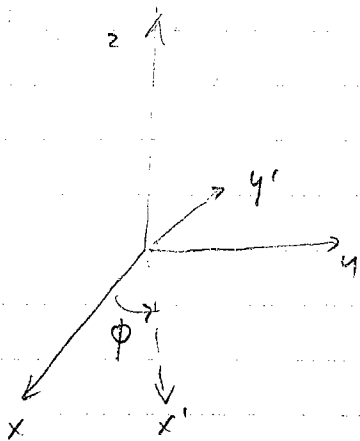
$$\left(\frac{d\vec{G}}{dt}\right)_{\mathcal{O}} = \left(\frac{d\vec{G}}{dt}\right)_{\mathcal{O}'} + \vec{\omega} \times \vec{G}$$

depending on application can be calculated in body or external frame

Schematically

$$\frac{d}{dt} = \frac{d}{dt}' + \vec{\omega} \times$$

$$\left(\frac{d\vec{G}}{dt}\right)_{\mathcal{O}} = \left(\frac{d\vec{G}}{dt}\right)_{\mathcal{O}'} + \vec{\omega} \times \vec{G}$$



Cartesian $\vec{\omega}'$ components in terms of Euler angular vel.

If only ψ finite

$$\omega_{z'} = \dot{\psi} \quad \omega_{x'} = \omega_{y'} = 0$$

If only ϕ finite

$$\omega_z = \dot{\phi} \quad \omega_x = \omega_y = 0$$

$$\omega_{z'} = \dot{\phi} \cos \theta$$

$$\omega_{y'} = \dot{\phi} \sin \theta \cos \psi$$

$$\omega_{x'} = \dot{\phi} \sin \theta \sin \psi$$

If only θ finite

$$\omega_{z'} = 0$$

$$\omega_{x'} = \dot{\theta} \cos \psi$$

$$\omega_{y'} = -\dot{\theta} \sin \psi$$

Overall, if all angles change

$$\omega_x' = \dot{\phi} \sin \theta \sin \psi + \dot{\theta} \cos \psi$$

$$\omega_y' = \dot{\phi} \sin \theta \cos \psi - \dot{\theta} \sin \psi$$

$$\omega_z' = \dot{\phi} \cos \theta + \dot{\psi}$$

Centrifugal and Coriolis Forces

$$\vec{v} = \vec{v}' + \vec{\omega} \times \vec{r}$$

\vec{v}' in system rotating at the frequency ω
 $\vec{\omega}$ fixed vector in other frame

$$\vec{a} = \frac{d\vec{v}}{dt} = \frac{d}{dt} (\vec{v}' + \vec{\omega} \times \vec{r}')_{g'} + \vec{\omega} \times (\vec{v}' + \vec{\omega} \times \vec{r}')$$

$$= \vec{a}' + \vec{\omega}' \times \vec{v}' + \vec{\omega} \times \vec{v}' + \vec{\omega} \times (\vec{\omega} \times \vec{r}')$$

$$= \vec{a}' + 2\vec{\omega} \times \vec{v}' + \vec{\omega} \times (\vec{\omega} \times \vec{r}')$$

$$\vec{F} = m\vec{a} = m\vec{a}' + 2m\vec{\omega} \times \vec{v}' + m\vec{\omega} \times (\vec{\omega} \times \vec{r}')$$

$$m\vec{a}' = \vec{F}_{\text{eff}} = \vec{F} - \underbrace{m\vec{\omega} \times (\vec{\omega} \times \vec{r}')}_{\vec{F}_c} - \underbrace{2m(\vec{\omega} \times \vec{v}')}_{\vec{F}_{\text{Cor}}}$$

↑
effective force
in a rotating
system

↑
centrifugal
force

↑
Coriolis
force

The Coriolis force is present if the particle moves in the rotating frame.

The centrifugal force is present irrespective of a motion.

$$\vec{F}_{cf} = -m \vec{\omega} \times (\vec{\omega} \times \vec{r})$$

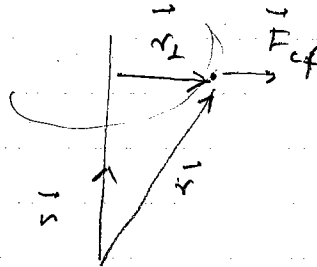
follows from the identity for antisym symbol in tensor notation

$$\vec{A} \times (\vec{B} \times \vec{C}) = (\vec{A} \cdot \vec{C}) \vec{B} - (\vec{A} \cdot \vec{B}) \vec{C}$$

$$\vec{F}_{cf} = -m [(\vec{\omega} \cdot \vec{r}) \vec{\omega} - \omega^2 \vec{r}]$$

$$= m \omega^2 [\vec{r} - \vec{n} (\vec{n} \cdot \vec{r})] = m \omega^2 \vec{r}_\perp$$

$$\vec{F}_{cf} \perp \vec{\omega}, \vec{n}$$

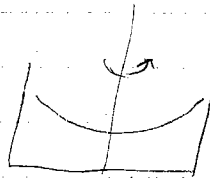


demos

container
w/water



→



The surface of the water will align with the equipotential surface for the effective force in the rotating system, if such surface exists

$$\vec{F}_{ef} = m \vec{g} - m \vec{\omega} \times (\vec{\omega} \times \vec{r}) = m \vec{g}_{ef}$$

↑ small amount of water

$$\vec{g}_{ef} = \vec{g} - m \vec{\omega} \times (\vec{\omega} \times \vec{r})$$

effective gravitational acceleration

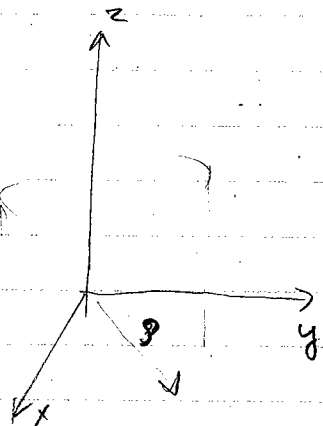
surface of the water needs to be locally \perp to \vec{g}_{ef} .

←

The effective force needs to be \perp to the surface of the water in the rotating frame

Otherwise the water can accelerate along the surface to the change in the surface shape.

Exercise: Determine the shape for the surface of water in a ^{cylindrical} rotating pail.



$$\vec{F}_{ef} = -mg \vec{u}_z + m\omega^2 \rho \vec{u}_\rho$$

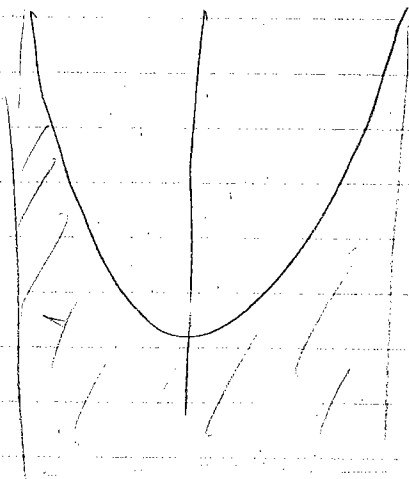
$$\vec{F}_{ef} = -\nabla V_{ef}$$

$$V_{ef} = mgz - \frac{1}{2} m\omega^2 \rho^2 + V_0$$

surface of constant V :

$$V_{ef} = mgz - \frac{1}{2} m\omega^2 \rho^2 + V_0 = \text{const}$$

$$z = \frac{\omega^2}{2g} \rho^2 + z_0 \quad \text{eq. of paraboloid}$$



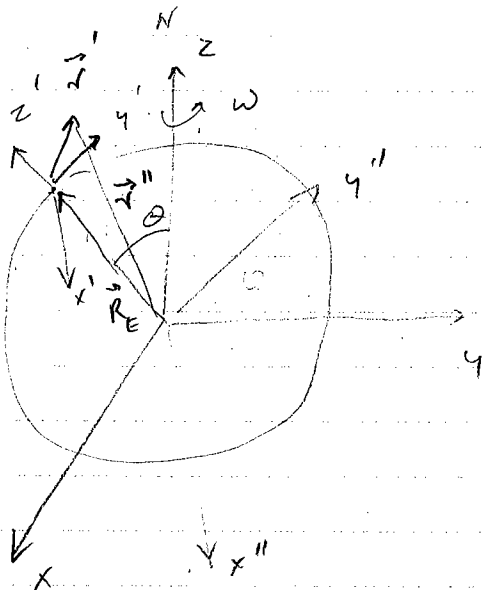
Newton observing the surface of water in a rotating pail's came up with the concepts of inertial and noninertial frames of reference

Sun moves towards West

Earth rotates towards East

θ & θ' origin at Earth's center θ' at surface

Motion on the Earth



θ - colatitude

Note: axes not quite aligned!

angle

$$\omega = \frac{2\pi}{24 \times 3600} \times \frac{366.25}{365.25}$$

actual # of rotations
(in the apparent one taken up by the rotation around the sun)

apparent # of rotations per year

deviation of a year in sec

$$= 7.292 \times 10^{-5} \text{ s}^{-1}$$

$$\frac{\vec{F}_c}{m} = \vec{g}_{eff} = \vec{g} + \omega^2 \vec{r}_\perp \approx \vec{g} + \omega^2 \vec{R}_{E\perp}$$

$$\Delta g = \omega^2 R_\perp = \omega^2 R_E \sin \theta$$

$\approx 0.3\% g$

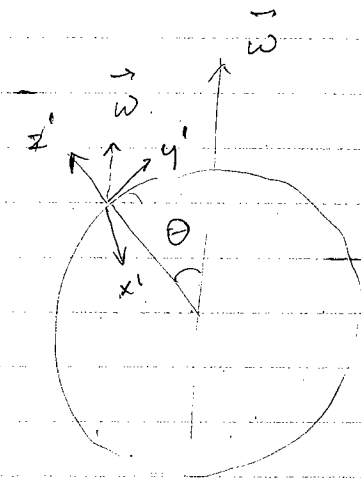
$$\omega^2 R_E = 5 \times 10^{-9} \text{ s}^{-2} \times 6 \times 10^6 \text{ m} = 0.03 \frac{\text{m}}{\text{s}^2}$$

actually $R_E = 6,371 \text{ km}$

$$R_E = \frac{2\pi R_E}{2\pi} = \frac{4 \times 10^7 \text{ m}}{2\pi} = 6.4 \times 10^6 \text{ m}$$

Small, causes a finite bulging of Earth surface aligning with the equipotential surface of \vec{V}_{eff}

The Coriolis force



$$\omega_{z'} = \omega \cos \theta$$

$$\omega_{y'} = \omega \sin \theta$$

$$\omega_{x'} = 0$$

$$\vec{F}_{\text{Cor}} = -2m \vec{\omega} \times \vec{v}'$$

$$= 2m \vec{v}' \times \vec{\omega}$$

$$\begin{vmatrix} \vec{u}_{x'} & \vec{u}_{y'} & \vec{u}_{z'} \\ v_{x'} & v_{y'} & v_{z'} \\ 0 & \omega \sin \theta & \omega \cos \theta \end{vmatrix}$$

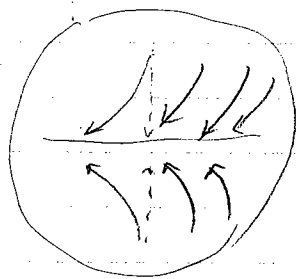
$$\vec{F}_{\text{Cor}} = 2m \omega \left[(v_{y'} \cos \theta - v_{z'} \sin \theta) \vec{u}_{x'} - v_{x'} \cos \theta \vec{u}_{y'} + v_{x'} \sin \theta \vec{u}_{z'} \right]$$

Velocity dir	Force	N hemisphere $\theta < \frac{\pi}{2}$
N $v_{y'} > 0$	East	
E $v_{x'} > 0$	South + Up	
S $v_{y'} < 0$	West	
W $v_{x'} < 0$	North + Down	
U $v_{z'} > 0$	West	
D $v_{z'} < 0$	East	

For motion \vec{u} to earth's surface, the pticle is always deflected to the right in N hemisphere and to the left in the S hemisphere, I.e., the direction is to oppose a rotation with the frame.

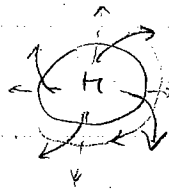
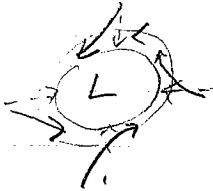
Wind patterns are striking examples of the effects of the Coriolis force

Global pattern. Heated air at the equator rises up. ^{Coolest} Air from northern regions comes in



prevailing wind direction
SW

Smaller scale patterns



Typhoon
hurricane