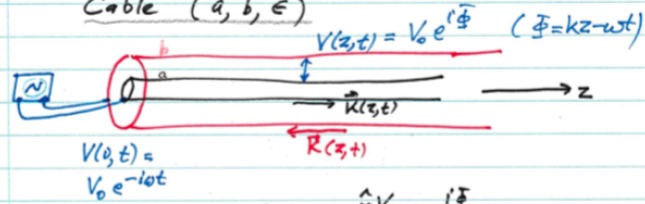


enter

z

### Line Impedance of a coaxial Cable (a, b, ε)



$$V(z,t) = V_0 e^{i\Phi} \quad (\Phi = kz - \omega t)$$

$$V(z,t) = V_0 e^{-i\omega t}$$

$$\vec{E}(z,t) = \frac{\hat{r} V_0}{r \ln(b/a)} e^{i\Phi}$$

$$\vec{B}(z,t) = \frac{\hat{\phi} V_0 e^{i\Phi}}{v r \ln(b/a)} \quad \text{where } v = \frac{1}{\sqrt{\mu_0 \epsilon}}$$

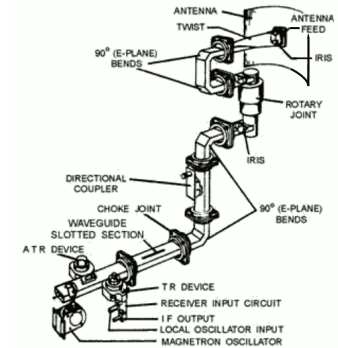
$$\vec{K}(z,t) = \frac{\hat{r} \times \vec{B}}{\mu_0} \quad (\Delta H_z = K)$$

$$\vec{K}(z,t) = \frac{\hat{z} V_0 e^{i\Phi}}{\mu_0 v a \ln(b/a)}$$

$$I(z,t) = \oint K_z \, a \, d\phi = \frac{V_0 - 2\pi e^{i\Phi}}{\mu_0 v \ln(b/a)}$$

$$Z = \frac{V}{I} = \frac{V_0 e^{i\Phi} \mu_0 v \ln(b/a)}{V_0 \cdot 2\pi e^{i\Phi}} = \frac{\ln(b/a)}{2\pi} \sqrt{\frac{\mu_0}{\epsilon}}$$

GraphicsGrid[{{wg, RD}}]



I'm not sure why we are studying waveguides, but it is included in the PHY 842 course description.

A coaxial cable is a transmission line.

Sometimes a waveguide is better than a coaxial cable (why?) (homework question)

## Waveguides

### -boundary conditions (Section 8.1)

The calculation of the TEM mode of a coaxial cable shows the importance of boundary conditions.

We assumed that the conductors are perfect conductors, so  $\mathbf{E} = 0$  and  $\mathbf{B} = 0$  inside the conductor.

What about real metals?

Jackson :

*“A good conductor behaves effectively like a perfect conductor, with the idealized surface current replaced by an equivalent surface current, which is actually distributed throughout a small thickness at the surface.”*

Read Jackson Section 8.1: “Fields at the surface of and inside a conductor”

### Perfect conductor

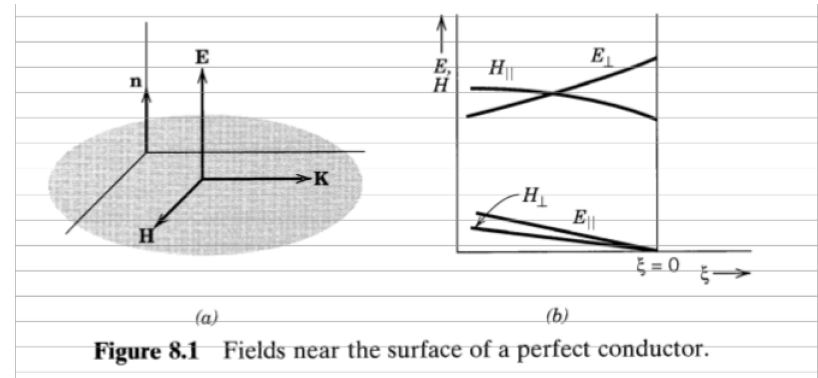


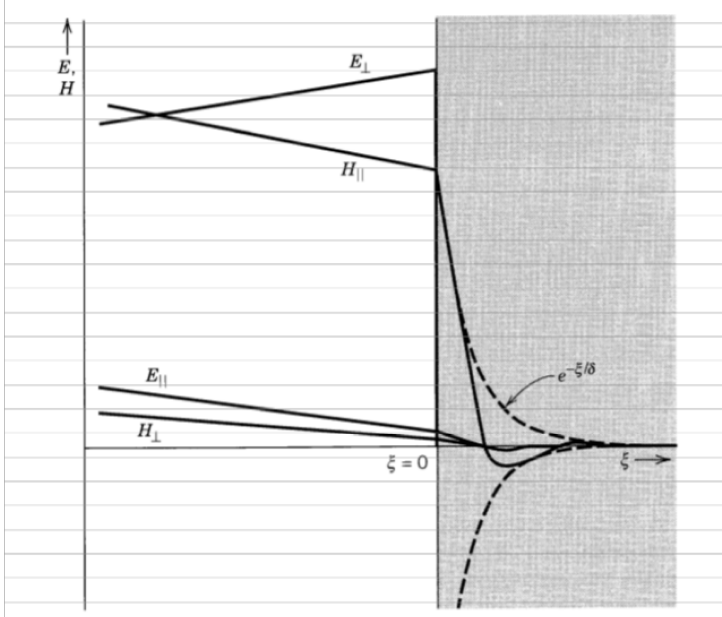
Figure 8.1 Fields near the surface of a perfect conductor.

The shaded region is a small area on the conductor surface;  $\hat{n}$  = unit normal;  
 $\rightarrow \mathbf{K}$  = surface current density;  
 $\rightarrow \mathbf{E} = 0$  and  $\rightarrow \mathbf{H} = 0$  in the perfect conductor,  
 so  $\rightarrow \mathbf{E}$  is normal and  $\rightarrow \mathbf{H}$  is tangential at the outer surface.

For a real metal, the conductivity  $\sigma$  is large but finite; so the skin depth  $\delta = \sqrt{2/(\mu_0 \omega \sigma)}$  is small .

Figure 8.1  
(perfect conductor;  $\sigma = \infty$ ,  $\delta = 0$ )  
Figure 8.2  
(good conductor;  $\delta$  is "small" )

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We'll analyze waveguides in a two-step calculation called "successive approximations":

▪ First we solve the problem for the ideal conductor; i.e.,  $\sigma \rightarrow \infty$ . Here the boundary conditions are

$$\hat{n} \cdot \vec{B} = 0 \quad \text{and} \quad \hat{n} \times \vec{E} = 0$$

$$\hat{n} \cdot \vec{D} = \Sigma \quad \text{and} \quad \hat{n} \times \vec{H} = \vec{K}$$

where  $\Sigma$  = ideal surface charge density and  $\vec{K}$  = ideal surface current density.

That idealization means that  $\vec{E}$  and  $\vec{B}$  are 0 inside the conductors — the first approximation.

▪ Then, to calculate energy loss from electrical resistance, we'll calculate the fields in a thin layer just inside the conductor — the second approximation. These are the results from Jackson ...

$$\vec{H}_c = \vec{H}_{\parallel} e^{-\xi/\delta} e^{-i\xi/\delta},$$

where  $\xi$  = distance inside C.

and  $H_{\parallel}$  = tangential field at the surface

$$\vec{E}_c = \sqrt{\frac{\mu_c \omega}{2\sigma}} (1-i)(\hat{n} \times \vec{H}_{\parallel}) e^{-\xi/\delta} e^{i\xi/\delta},$$

At the outer surface we can approximate  $E_{\text{normal}} = \Sigma/\epsilon$  and  $H_{\text{tang.}} = K_{\text{eff}}$ ; and we can neglect  $H_{\text{normal}}$  and  $E_{\text{tang.}}$ ; see Figure 8.2 and Equation 8.11:

$$\vec{E}_{\parallel} = \sqrt{\frac{\mu_c \omega}{2\sigma}} (1-i)(\hat{n} \times \vec{H}_{\parallel})$$

### ■ Power loss

The guided wave loses energy.

Power loss = the power flowing through the surface of the conductor.

$$\begin{aligned} \left\langle \frac{dP_{\text{loss}}}{da} \right\rangle &= -\frac{1}{2} \text{Re}\{ \hat{n} \cdot \vec{E} \times (\vec{H})^* \} \\ &= \frac{\mu_c \omega \delta}{4} |\vec{H}_{\parallel}|^2 \end{aligned}$$

where  $\langle \dots \rangle$  means time averaged

The “loss of energy” is due to resistance of the conductor (finite  $\sigma$ ); ohmic loss; current density in the conductor,  $\vec{J} = \sigma \vec{E}_c$ .

■ OR, in terms of the “surface current”,

$$\begin{aligned} \vec{K}_{\text{eff}} &= \int_0^{\infty} \vec{J} d\xi = \hat{n} \times \vec{H}_{\parallel} \\ \left\langle \frac{dP_{\text{loss}}}{da} \right\rangle &= \frac{1}{2\sigma\delta} |\vec{K}_{\text{eff}}|^2 \end{aligned}$$



## Cylindrical waveguides (Section 8.2)

Figure 8.3

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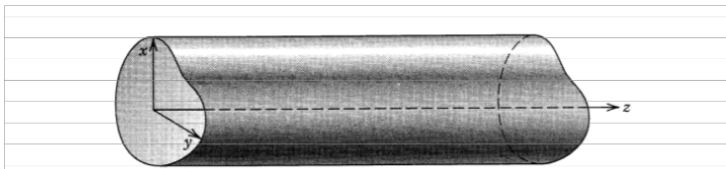


Figure 8.3 Hollow, cylindrical waveguide of arbitrary cross-sectional shape.

Field equations for harmonic time dependence,  $F(\vec{x}, t) = F(\vec{x}) e^{-i\omega t}$ ,

$$\text{curl } \vec{E} = i\omega \vec{B} \quad \text{and} \quad \text{div } \vec{B} = 0$$

$$\text{curl } \vec{B} = -i\mu\epsilon\omega \vec{E} \quad \text{and} \quad \text{div } \vec{E} = 0$$

We know that these imply

$$(\nabla^2 + \mu\epsilon\omega^2) \{ \vec{E} \text{ and } \vec{B} \} = 0$$

Using the symmetry —  
translation invariance in  $z$  —  
we'll consider waves propagating down  
the wave guide,

$$\vec{E}(\vec{x}, t) = \vec{E}(x, y) e^{i(kz - \omega t)}$$

$$\vec{B}(\vec{x}, t) = \vec{B}(x, y) e^{i(kz - \omega t)}$$

Remember, many kinds of superpositions  
are possible.

Now,

$$(\nabla_T^2 - k^2 + \mu\epsilon\omega^2) (\vec{E} \text{ and } \vec{B}) = 0$$

$$\text{where } \nabla_T^2 = \partial_x^2 + \partial_y^2.$$

So, we have a 2D partial differential equation to solve inside the waveguide, along with appropriate boundary conditions.

## The boundary value problem for a hollow waveguide

There are two types of solution.

TE = transverse electric:  $E_z(x,y) = 0$

TM = transverse magnetic:  $B_z(x,y) = 0$

For a waveguide in the form of a hollow cylinder, there are no TEM waves!

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The final consequence is that the TEM mode cannot exist inside a single, hollow, cylindrical conductor of infinite conductivity. The surface is an equipotential; the electric field therefore vanishes inside. It is necessary to have two or more cylindrical surfaces to support the TEM mode. The familiar coaxial cable and the parallel-wire transmission line are structures for which this is the dominant mode. (See Problems 8.1 and 8.2.)

## TM modes; $B_z = 0$

$$\vec{B} = \vec{B}_T(x,y) e^{ikz} e^{-i\omega t}$$

$$\vec{E} = [\vec{E}_T(x,y) + \hat{e}_z E_z(x,y)] e^{ikz} e^{-i\omega t}$$

Please verify ...

TM modes	$B_z = 0$
$\nabla \cdot \mu \vec{H} = 0$	$\nabla_T \cdot \vec{H}_T = 0$
$\nabla \cdot \epsilon \vec{E} = 0$	$\nabla_T \cdot \vec{E}_T + ik E_z = 0$
$i\omega \mu \vec{H} = \nabla \times \vec{E}$	$0 = \hat{e}_z \cdot (\nabla_T \times \vec{E}_T)$
,	$i\omega \mu \vec{H}_T = -\hat{e}_z \times \nabla_T E_z - ik \hat{e}_z \times \vec{E}_T$
$-i\omega \epsilon \vec{E} = \nabla \times \vec{H}$	$-i\omega \epsilon E_z = \hat{e}_z \cdot (\nabla_T \times \vec{H}_T)$
,	$-i\omega \epsilon \vec{E}_T = -ik \hat{e}_z \times \vec{H}_T$

These are PDE's. What are the boundary conditions?  $E_{\text{tangential}}$  is continuous, and it is 0 in the conductor; so  $E_z|_S = 0$ .

Since  $\nabla_T \times \vec{E}_T = 0$  we can write

$$\vec{E}_T = \frac{ik}{\gamma^2} \nabla_T \psi .$$

By the wave equation,

$$(\nabla_T^2 - k^2 + \mu\epsilon\omega^2) \psi = 0$$

$$= (\nabla_T^2 + \gamma^2) \psi$$

$$\text{where } \gamma^2 \equiv \mu\epsilon\omega^2 - k^2$$

We also have

$$ik E_z = -\nabla_T \cdot \vec{E}_T \implies E_z = \frac{-1}{\gamma^2} \nabla_T^2 \psi = \psi;$$

this implies the boundary condition

$$\psi|_S = 0 .$$

Wave equation + boundary condition  
 $\implies$  eigenvalues and eigenfunctions.

### TE modes ; $E_z = 0$

Please verify ...

TE modes	$E_z = 0$
$\nabla \cdot \mu \vec{H} = 0$	$\nabla_T \cdot \vec{H}_T + ik H_z = 0$
$\nabla \cdot \epsilon \vec{E} = 0$	$\nabla_T \cdot \vec{E}_T = 0$
$i\omega \mu \vec{H} = \nabla \times \vec{E}$	$i\omega \mu H_z = \hat{e}_z \cdot (\nabla_T \times \vec{E}_T)$
,	$i\omega \mu \vec{H}_T = -ik \hat{e}_z \times \vec{E}_T$
$-i\omega \epsilon \vec{E} = \nabla \times \vec{H}$	$0 = \hat{e}_z \cdot (\nabla_T \times \vec{H}_T)$
,	$-i\omega \epsilon \vec{E}_T = \hat{e}_z \times \nabla_T H_z - ik \hat{e}_z \times \vec{H}_T$

Write  $\vec{H}_T = \frac{ik}{\gamma^2} \nabla_T \psi$ . Then show  $H_z = \psi$ .

The boundary condition:  $B_{\text{normal}}$  is continuous at S and =0 in the conductor;

$\therefore \mathbf{n} \cdot \mathbf{H}_T = 0$  on the surface S;

this implies  $\mathbf{n} \cdot \nabla_T \psi = 0$ ; or,  $(\partial\psi/\partial n)|_S = 0$ .

# Modes of propagation in a rectangular waveguide

Out:-

